

EMD-Based Signal Filtering

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Abstract—In this paper, a signal-filtering method based on empirical mode decomposition is proposed. The filtering method is a fully data-driven approach. A noisy signal is adaptively decomposed into intrinsic oscillatory components called intrinsic mode functions (IMFs) by means of an algorithm referred to as a sifting process. The basic principle of the method is to make use of partial reconstructions of the signal, with the relevant IMFs corresponding to the most important structures of the signal (low-frequency components). A criterion is proposed to determine the IMF, after which, the energy distribution of the important structures of the signal overcomes that of the noise and that of the high-frequency components of the signal. The method is illustrated on simulated and real data, and the results are compared to well-known filtering methods. The study is limited to signals that were corrupted by additive white Gaussian noise and is conducted on the basis of extended numerical experiments.

Index Terms—Empirical mode decomposition (EMD), nonstationary signals, signal filtering.

I. INTRODUCTION

THE RECOVERY of a signal from observed noisy data, while preserving its important features (e.g., smoothness), remains a challenging problem in both signal processing and statistics. A number of filtering methods have been proposed, particularly for the case of additive white Gaussian noise (AWGN) [1]–[3]. Frequently, linear methods such as the Wiener filtering [1] are used because linear filters are easy to design and implement. However, linear filtering methods are not very effective when signals contain sharp edges and impulses of short duration. Furthermore, real signals are often nonstationary. To overcome these shortcomings, nonlinear methods have been proposed, particularly those that are based on wavelet thresholding [2], [3]. The idea of wavelet thresholding relies on the assumption that signal magnitudes dominate the magnitudes of the noise in a wavelet representation so that wavelet coefficients can be set to zero if their magnitudes are less than a predetermined threshold [3]. A limit of the wavelet approach is that the basis functions are fixed and, thus, do not necessarily match all real signals. To avoid this problem, time–frequency atomic signal decomposition can be used [4], [5]. As for wavelet packets, if the dictionary is very large and rich with a collection of atomic waveforms, which are located

on a much finer grid in the time–frequency space than wavelet and cosine packet tables, then it should be possible to represent a large class of real signals (for denoising, compression, and so on). In spite of this, the basis functions must be specified (Gabor functions, damped sinusoids, and so on).

Recently, a new data-driven technique, referred to as empirical mode decomposition (EMD), has been introduced by Huang *et al.* [6] for analyzing data from nonstationary and nonlinear processes. The EMD has received more attention in terms of applications [7]–[17] and interpretations [18], [19]. The major advantage of the EMD is that the basis functions are derived from the signal itself. Hence, the analysis is adaptive in contrast to the traditional methods where the basis functions are fixed. The EMD is based on the sequential extraction of energy associated with various intrinsic time scales of the signal, starting from finer temporal scales (high-frequency modes) to coarser ones (low-frequency modes). The total sum of the intrinsic mode functions (IMFs) matches the signal very well and, therefore, ensures completeness [6]. In our earlier paper, we have shown that the EMD can be used for signal denoising [10]. The method reconstructs the signal with all the IMFs that were previously thresholded, as in wavelet analysis, or filtered [10]. In this paper, the filtering scheme relies on the basic idea that most of the structures of the signal are often concentrated on lower frequency components (last IMFs) and decrease toward high-frequency modes (first IMFs). Thus, the recovered signal is reconstructed with only a few IMFs that are signal dominated. Consequently, compared to the approach introduced in [10], no thresholding or filtering is required. The proposed filtering method is a fully data-driven approach.

II. EMD ALGORITHM

The EMD involves the decomposition of a given signal $x(t)$ into a series of IMFs through the sifting process, with each one having a distinct time scale [6]. The decomposition is based on the local time scale of the signal and yields adaptive basis functions. The EMD can be seen as a type of wavelet decomposition whose subbands are built up as needed to separate the different components of $x(t)$. Each IMF then replaces the detail signals of $x(t)$ at a certain scale or frequency band [18]. The EMD picks out the highest frequency oscillation that remains in $x(t)$. A function is an IMF if R1) either the number of extrema and the number of zero crossings are equal or differ at most by one, and R2) at any point, the mean value of the envelope defined by the local maxima and the envelope defined by the local minima is zero. Thus, locally, each IMF contains lower frequency oscillations than the one that was extracted before. The EMD does not use any predetermined filter or wavelet function, and thus, it is a fully data-driven method [6]. To be

Manuscript received February 8, 2006; revised July 17, 2007.

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Digital Object Identifier 10.1109/TIM.2007.907967

successfully decomposed into IMFs, the signal $x(t)$ must have at least two extrema: one minimum and one maximum. The sifting process involves five major steps.

- Step 1) Fix $\epsilon, j \leftarrow 1$ (j th IMF).
- Step 2) $r_{j-1}(t) \leftarrow x(t)$ (residual).
- Step 3) Extract the j th IMF.
 - a) $h_{j,i-1}(t) \leftarrow r_{j-1}(t), i \leftarrow 1$ (i number of sifts).
 - b) Extract the local maxima/minima of $h_{j,i-1}(t)$.
 - c) Compute the upper and lower envelopes $U_{j,i-1}(t)$ and $L_{j,i-1}(t)$ by interpolating, using cubic spline, the local maxima and minima of $h_{j,i-1}(t)$, respectively.
 - d) Compute the envelope mean: $\mu_{j,i-1}(t) \leftarrow [U_{j,i-1}(t) + L_{j,i-1}(t)]/2$.
 - e) Update: $h_{j,i}(t) \leftarrow h_{j,i-1}(t) - \mu_{j,i-1}(t), i \leftarrow i + 1$.
 - f) Calculate the stopping criterion by

$$SD(i) = \sum_{t=0}^N \frac{|h_{j,i-1}(t) - h_{j,i}(t)|^2}{[h_{j,i-1}(t)]^2}.$$

- g) Repeat Steps b)–f) until $SD(i) < \epsilon$, and then, put $\text{IMF}_j(t) \leftarrow h_{j,i}(t)$ (j th IMF).

Step 4) Update the residual: $r_j(t) \leftarrow r_{j-1}(t) - \text{IMF}_j(t)$.

Step 5) Repeat Step 3 with $j \leftarrow j + 1$ until the number of extrema in $r_j(t)$ is < 2 .

Here, N is the time duration. The “ $a \leftarrow b$ ” arrow is an assignment or a substitution operation; it means that the value of the variable a is to be replaced by the current value of the variable b . The sifting is repeated several times (i) to get h to be a true IMF that fulfills requirements R1) and R2). The result of the sifting is that $x(t)$ will be decomposed into $\text{IMF}_j(t), j = 1, \dots, C$, and a residual $r_C(t)$ given by

$$x(t) = \sum_{j=1}^C \text{IMF}_j(t) + r_C(t) \quad (1)$$

where C is the number of modes, which is automatically determined using the stopping criterion SD [Step 3)–f)]. Thus, C is signal dependent. The sifting process has two effects: 1) It eliminates riding waves, and 2) it smoothes uneven amplitudes. To guarantee that the IMF components will retain enough physical sense of both amplitude and frequency modulations, we have to determine a criterion for the sifting process to stop. This is accomplished by limiting the size of the standard deviation SD computed from the two consecutive sifting results. Usually, SD is set between 0.2 and 0.3 [6].

III. FILTERING APPROACH

The filtering method relies on the basic idea that most of the important structures of the signal are often concentrated on the lower frequency ones (last IMFs) and decrease toward high-frequency modes (first IMFs). Thus, one can assume that, for many signal classes that are corrupted by white noise, the signal-to-noise ratio (SNR) is higher at low frequencies than at high ones. According to this idea, there will be a mode indexed by j_s , after which, the energy distribution of the important structures of the signal overcomes that of the

noise and that of the high-frequency components of the signal. This particular mode $\text{IMF}_{j_s}(t)$ allows us to retrieve the most important structures of the signal from its noisy version. The modes after $\text{IMF}_{j_s}(t)$ are dominated by the signal, whereas the previous modes are high-frequency component dominated. In the proposed method, high-frequency-dominated modes are set to zero (hard thresholding) and will not be used in the signal reconstruction. The signal is partially reconstructed. The problem of reducing noise is complicated and difficult because the noise level in the signal is unknown. Furthermore, analytical expressions of the signal IMFs are not available. Most of the important results on the EMD are all based on the empirically determined findings from numerical experiments [6], [18], [19]. Thus, the filtering problem is empirically studied.

Consider a deterministic signal $y(t)$ corrupted by an AWGN as follows:

$$x(t) = y(t) + z(t). \quad (2)$$

From this observed signal $x(t)$, the objective is to find an approximation $\tilde{y}(t)$ to the original signal $y(t)$ that minimizes the mean square error (MSE) given by

$$\text{MSE}(y, \tilde{y}) \triangleq \frac{1}{N} \sum_{i=1}^N [y(t_i) - \tilde{y}(t_i)]^2 \quad (3)$$

where $y = [y(t_1), y(t_2), \dots, y(t_N)]^T$, and $\tilde{y} = [\tilde{y}(t_1), \tilde{y}(t_2), \dots, \tilde{y}(t_N)]^T$. Here, N is the length of the signal. Other distortion measures such as the mean absolute error (MAE) can be used [3]. Then, $x(t)$ is first decomposed using the EMD (1) into $\text{IMF}_j(t), j = 1, \dots, C$, and a residual $r_C(t)$, and finally, $\tilde{y}(t)$ is reconstructed using $(C - k + 1)$ -selected IMFs, starting from k to C , as follows:

$$\tilde{y}_k(t) = \sum_{j=k}^C \text{IMF}_j(t) + r_C(t), \quad k = 2, \dots, C. \quad (4)$$

The aim of the EMD filtering is to find the index $k = j_s$ that minimizes the $\text{MSE}(y, \tilde{y})$. In practice, the mse or the MAE cannot be calculated because the original signal $y(t)$ is unknown. In this paper, we propose a distortion measure, called consecutive mse (CMSE), that does not require any knowledge of $y(t)$. This quantity measures the squared Euclidean distance between two consecutive reconstructions of the signal. The CMSE is defined as follows:

$$\begin{aligned} \text{CMSE}(\tilde{y}_k, \tilde{y}_{k+1}) & \triangleq \frac{1}{N} \sum_{i=1}^N [\tilde{y}_k(t_i) - \tilde{y}_{k+1}(t_i)]^2, \quad k = 1, \dots, C - 1 \quad (5) \\ & \triangleq \frac{1}{N} \sum_{i=1}^N [\text{IMF}_k(t_i)]^2. \quad (6) \end{aligned}$$

Thus, according to (6), the CMSE is reduced to the energy of the k th IMF. It is also the classical empirical variance estimate of the IMF [if $k = 1, \tilde{y}_k(t) = x(t)$]. Finally, the index j_s is given by

$$j_s = \arg \min_{1 \leq k \leq C-1} [\text{CMSE}(\tilde{y}_k, \tilde{y}_{k+1})] \quad (7)$$

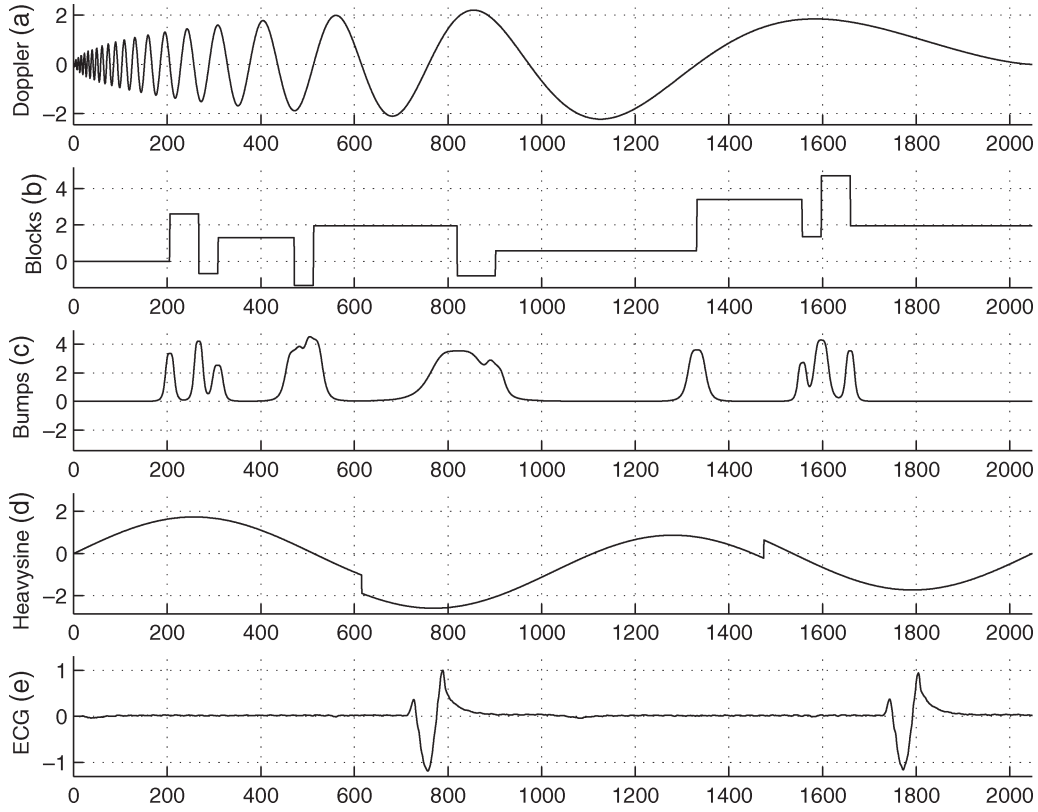


Fig. 1. Test signals with $N = 2048$.

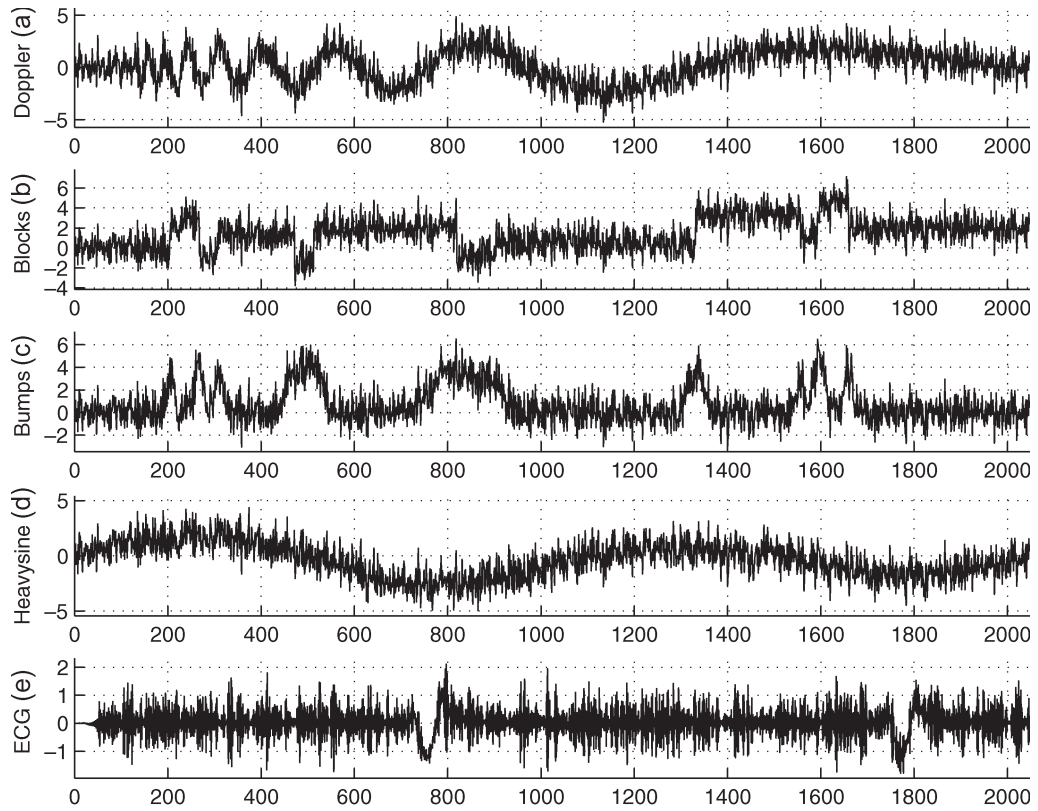


Fig. 2. Noisy test signals (SNR = 2 dB; SNR = -9 dB for ECG).

where \tilde{y}_k and \tilde{y}_{k+1} are signals that are reconstructed starting from the IMFs that are indexed by k and $(k + 1)$, respectively. The criterion CMSE allows for the identification of

the IMF order where there is the first significant change in energy. This empirical fact is derived from extended numerical experiments.

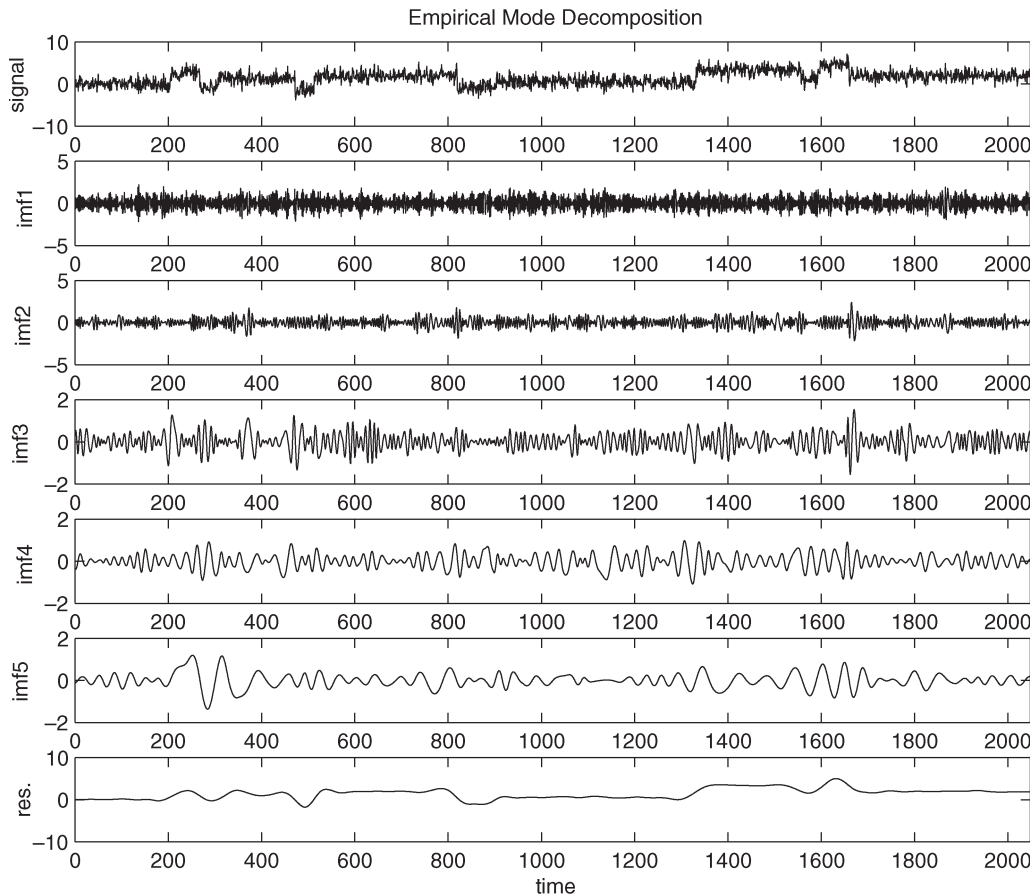


Fig. 3. EMD of the noisy “Blocks” signal. The decomposition performed by the EMD is given in the five IMFs that are plotted in the lower part, with the last row corresponding to the final residue.

A. Filtering Algorithm

The EMD filtering consists of six different steps.

- Step 1) Fix SD (usually between 0.2 and 0.3 [6]).
- Step 2) Run the sifting to extract the IMF_k $k = 1, \dots, C - 1$ of $x(t)$.
- Step 3) Compute $\tilde{y}_k(t)$, for $k = 1, \dots, C - 1$, using (4).
- Step 4) Compute $CMS(\tilde{y}_k, \tilde{y}_{k+1})$, for $k = 1, \dots, C - 1$, using (6).
- Step 5) Compute j_s using (7).
- Step 6) Reconstruct $\tilde{y}_{j_s}(t)$, which is the filtered signal, using (4).

IV. RESULTS AND DISCUSSIONS

To test the EMD filtering method, we have performed numerical simulations for four test signals: 1) “Doppler,” 2) “Blocks,” 3) “Bumps,” and 4) “Heavysine.” These were obtained using the WAVELAB software.¹ The time duration of these signals is 1 s, and the size is $N = 2048$. The method is also tested on two real signals: 1) a biomedical signal, i.e., electrocardiogram (ECG), and 2) a real turbulent pressure signal derived from a fluid mechanics system. The “ECG” and the turbulent signal are collected using sampling frequencies of 1 and 20 kHz,

¹Available from Stanford Statistics Department, courtesy of D. L. Donoho and I. M. Johnstone.

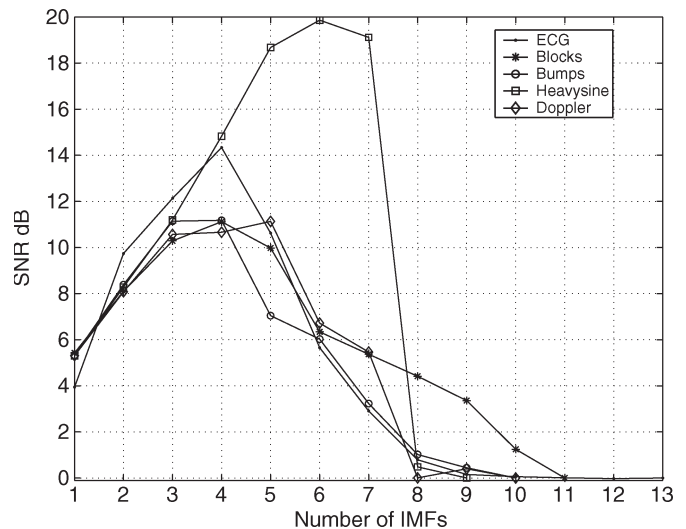


Fig. 4. Dependencies of the SNR values versus the number of IMFs for the five signals.

respectively. MSE and SNR are calculated as the measures of efficiency of noise reduction. For synthesized signals, the variance of the AWGN is set so that the original SNR (before filtering) is maintained at 2 dB. The SNR of the “ECG” is -9 dB. The original signals and the corresponding noisy versions are depicted in Figs. 1 and 2, respectively [10]. The only parameter used to run the EMD filtering is the stopping criterion SD ,

TABLE I
C AND j_s VALUES OF EACH TEST SIGNAL

Signals	“Doppler”	“Blocks”	“Heavysine”	“Bumps”	“ECG”
C	10	11	9	10	13
J_s	5	4	6	4	4

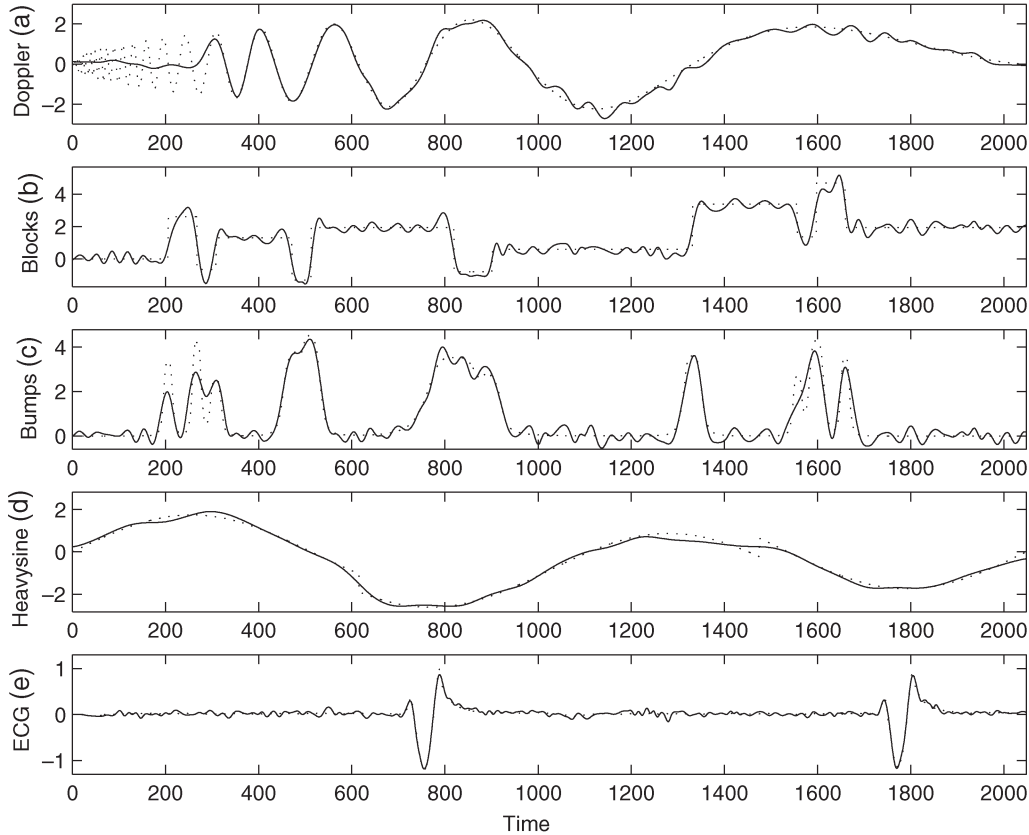


Fig. 5. Results of the EMD filtering. Free-noise signals (dotted line). Reconstructed signals (solid line).

TABLE II
FILTERING RESULTS OF THE DIFFERENT SIGNALS THAT WERE CORRUPTED BY THE GAUSSIAN NOISE

	“Doppler”		“Blocks”		“Bumps”		“Heavysine”		“ECG”	
	SNR	MSE	SNR	MSE	SNR	MSE	SNR	MSE	SNR	MSE
Noisy	2.06	1.04	2.03	1.04	2.03	1.04	2.03	1.04	-9.02	0.33
Averaging	9.86	0.17	9.06	0.20	9.46	0.19	12.66	0.09	7.23	8×10^{-3}
Median	10.57	0.15	10.17	0.16	10.55	0.15	10.67	0.15	4.62	14×10^{-3}
Wavelet	14.97	0.05	11.94	0.10	14.47	0.06	18.76	0.02	5.82	11×10^{-3}
EMD	11.13	0.12	11.97	0.09	11.18	0.12	19.86	0.02	14.33	1.5×10^{-3}

which is set to 0.25 [6]. Fig. 3 shows a sequential extraction of local oscillations by the EMD of the “Blocks” signal [Fig. 1(b)] [10]. The EMD decomposed the “Blocks” signal into 11 IMFs and a residual. Only five IMFs and the residual are represented. One can remark that the first IMF corresponds to a fast oscillation, whereas the fifth IMF corresponds to a slow one (Fig. 3). A comparison of the signal (top diagram) and the residue (bottom diagram) in Fig. 3 shows that the residue captures the trend of the signal. For the remaining signals, we obtained similar decompositions as in the “Blocks” signal. Thus, for an illustration of the method, we have restricted ourselves to the “Blocks” signal. The C values used in the reconstruction of the different signals are reported in Table I. Note that for the same

SD value, the C value is signal dependent. For the filtering scheme, each noisy signal is decomposed into IMFs, and the $j = j_s$ index is calculated using the CMSE minimum value (7). The filtered signals are constructed according to (4), where the signal is partially reconstructed using IMFs ranging from j_s to C (Table I), and the corresponding SNRs are estimated (Fig. 4). Fig. 4 shows the plots of the SNR values versus the number of IMFs for the five signals. The SNR maximum of each signal occurs at the j_s value (Table I). Note that each SNR plot exhibits a single hump. This fact is derived from extended numerical experiments. Fig. 5 displays the outcome of applying the EMD filtering scheme to the five signals. Each reconstructed signal plot (solid line) is superposed on the corresponding

free-noise signal (dotted line). Globally, the results are qualitatively appealing; the reconstructions jump where the true signal jumps and are smooth where the true signal is smooth. The significant results are obtained for the “Blocks,” “Heavysine,” and “ECG” signals [Fig. 5(b), (d), and (e)], which are very close to the original signals. These findings are confirmed by the SNR values listed in Table II, where significant improvements in the SNR range from 9.07 to 23.35 dB. Table II shows a comparison of the mse and SNR values for the averaging, median, wavelet, and EMD methods. For the median and averaging methods, different window sizes (3, 5, 7, 9, 11, and 13) are tested, and only the best results from these two methods are reported in Table II. For the wavelet method, the symmlet of Daubechies of the fifth order is used, followed by the soft thresholding of Donoho [3]. As indicated in Table II, our filtering scheme outperforms the averaging and median methods. For the “Heavysine” and “ECG” signals, our method performs better than the wavelet approach. However, the wavelet method performs better than the EMD filtering for the “Doppler” and “Bumps” signals. The efficiency of the compared methods depends on the signal behavior. In particular, for the ECG signal, the averaging method achieves a better SNR than the wavelet method. A careful examination of the “Doppler” signal [Fig. 5(a)] shows that the EMD scheme failed to correctly reconstruct the left part of the signal. This is expected because this signal part corresponds to a high-frequency component (rapid frequency changing) that has been set to zero during the reconstruction process. The oscillations that we see in Fig. 5 are particularly in the vicinity of discontinuities and other rapid changes. These are “Gibbs-like” oscillations caused by the fact that the signals (solid lines) are the partial reconstructions obtained using only a reduced number of IMFs. It is important to keep in mind that using a white noise implies that its components are distributed over all IMFs. Thus, the partial reconstruction scheme of the signal removes the high-frequency components of both the noise and the signal and leaves the low-frequency components of the noise. Consequently, one expects that if only the noisy parts of the first IMFs are set to zero, this will damp some of the oscillations and, consequently, improve the performance of the method. The oscillations seen in the flat regions [Fig. 5(b) and (c)] may be due to the interpolation scheme that was used (cubic spline), and thus, it would be interesting to search for interpolation methods other than cubic splines. The filtering scheme is also tested on another real signal derived from a fluid mechanics system. The pressure signal is acquired from the transient rotational motion of a hydrofoil in a transitional (laminar to turbulent) flow regime. The signal is recorded from a transducer located in a cavity on the hydrofoil’s suction side [17]. The EMD results in 11 IMFs and a residue. Fig. 6 shows the noisy signal (dotted line) above which is plotted the partial reconstruction of the signal (solid line) with $j_s = 10$ along with the residual (dashed line). This representation clearly shows the EMD-filtering effect on the noisy signal. The obtained EMD-filtered signal from the partial reconstruction not only conserves the overall trend of the signal but also allows to superpose it on as many high-frequency modes (IMFs), as needed, to represent the signal. The resulting representation is more suitable for analysis, and the desired data is conserved.

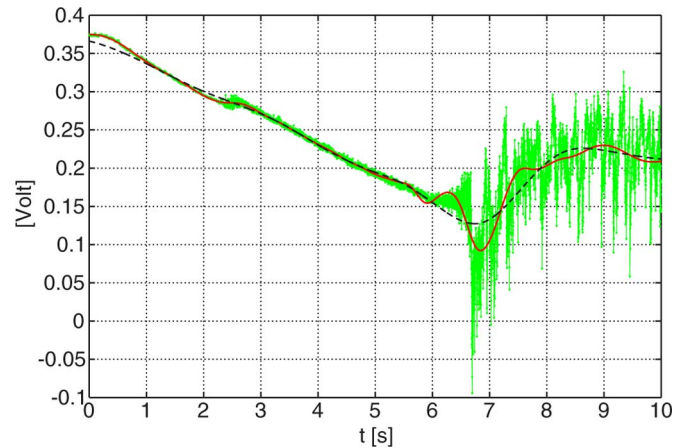


Fig. 6. EMD filtering of a real turbulent pressure signal derived from a fluid mechanics system. Noisy signal (dotted line). Residue (dashed line). Partial reconstruction with $j_s = 10$ and the residue (solid line).

V. CONCLUSION

This paper has presented a new signal-filtering method. The study is limited to the signals corrupted by the AWGN. This filtering scheme, which is based on the EMD method, is simple and fully data driven. The filtering scheme is based on the partial reconstruction of the signal using the IMFs that correspond to the most important structures of the signal (low-frequency modes). The method does not use any preprocessing or post-processing and does not require any user parameter setting. The results that have been obtained for the synthetic signals and for one real signal indicate that our method is effective for noise removal. Because the current status of the EMD still lacks theoretical grounds, the present study has been conducted on the basis of extended numerical experiments. The method is more effective for very noisy signals and where noise-level estimation is not possible. Our method outperforms the averaging and median methods, and for two signals, it performs better than the wavelet method. To confirm the effectiveness of the EMD filtering, the method must be evaluated with a large class of signals and in different experimental conditions such as noise levels, sampling rates, and sample sizes. In future work, we plan to extend this study to other noise models, such as the fractional Gaussian noise, and investigate the effect of sampling on the EMD.

ACKNOWLEDGMENT

The authors would like to thank the Associate Editor and the reviewers for their very helpful comments and suggestions that improved this paper, as well as Dr. S. Benramdane from Ecole Navale (Brest Armées, France), for the many fruitful discussions and for providing real data (Fig. 6).

REFERENCES

- [1] J. G. Proakis and D. G. Manolakis, *Digital Signal Processing: Principles, Algorithms, and Applications*, 3rd ed. Englewood Cliffs, NJ: Prentice-Hall, 1996.
- [2] D. L. Donoho and I. M. Johnstone, “Ideal spatial adaptation via wavelet shrinkage,” *Biometrika*, vol. 81, pp. 425–455, 1994.
- [3] D. L. Donoho, “De-noising by soft-thresholding,” *IEEE Trans. Inf. Theory*, vol. 41, no. 3, pp. 613–627, May 1995.

- [4] S. Mallat and Z. Zhang, "Matching pursuits with time-frequency dictionaries," *IEEE Trans. Signal Process.*, vol. 41, no. 12, pp. 3397–3415, Dec. 1993.
- [5] M. M. Goodwin and M. Vetterli, "Matching pursuit and atomic signal models based on recursive filter banks," *IEEE Trans. Signal Process.*, vol. 47, no. 7, pp. 1890–1901, Jul. 1999.
- [6] N. E. Huang, Z. Shen, S. R. Long, M. C. Wu, H. H. Shin, Q. Zheng, N. C. Yen, C. C. Tung, and H. H. Liu, "The empirical mode decomposition and the Hilbert spectrum for nonlinear and non-stationary time series analysis," *Proc. R. Soc. Lond. A, Math. Phys. Sci.*, vol. 454, no. 1971, pp. 903–995, Mar. 1998.
- [7] A. O. Boudraa, J. C. Cexus, F. Salzenstein, and L. Guillon, "IF estimation using empirical mode decomposition and nonlinear Teager energy operator," in *Proc. IEEE ISCCSP*, Hammamet, Tunisia, 2004, pp. 45–48.
- [8] J. C. Cexus and A. O. Boudraa, "Nonstationary signals analysis by Teager–Huang transform (THT)," in *Proc. EUSIPCO*, Florence, Italy, 2006, 5 p.
- [9] J. C. Cexus and A. O. Boudraa, "Teager–Huang analysis applied to sonar target recognition," *Int. J. Signal Process.*, vol. 1, no. 1, pp. 23–27, 2004.
- [10] A. O. Boudraa, J. C. Cexus, and Z. Saidi, "EMD-based signal noise reduction," *Int. J. Signal Process.*, vol. 1, no. 1, pp. 33–37, 2004.
- [11] Z. Liu and S. Peng, "Boundary processing of bidimensional EMD using texture synthesis," *IEEE Signal Process. Lett.*, vol. 12, no. 1, pp. 33–36, Jan. 2005.
- [12] A. O. Boudraa, J. C. Cexus, F. Salzenstein, and A. Beghdadi, "EMD-based multibeam echosounder images segmentation," in *Proc. IEEE ISCCSP*, Marrakech, Morocco, 2006.
- [13] K. Zeng and M. X. He, "A simple boundary process technique for empirical mode decomposition," in *Proc. IEEE IGARSS*, 2004, vol. 6, pp. 4258–4261.
- [14] P. Flandrin, P. Goncalves, and G. Rilling, "Detrending and denoising with empirical mode decompositions," in *Proc. EUSIPCO*, Vienna, Austria, 2004, pp. 1581–1584.
- [15] G. Rilling, P. Flandrin, and P. Goncalves, "Empirical mode decomposition, fractional Gaussian noise, and Hurst exponent estimation," in *Proc. IEEE ICASSP*, Philadelphia, PA, 2005, vol. 4, pp. 489–492.
- [16] R. Deering and J. F. Kaiser, "The use of a masking signal to improve empirical mode decomposition," in *Proc. IEEE ICASSP*, Philadelphia, USA, 2005, vol. 4, pp. 485–488.
- [17] S. Benramdane, J. C. Cexus, A. O. Boudraa, and J. A. Astolfi, "Transient turbulent pressure signal processing using empirical mode decomposition," in *Proc. Phys. Signal Image Process.*, Mulhouse, France, 2007.
- [18] P. Flandrin, G. Rilling, and P. Goncalves, "Empirical mode decomposition as a filter bank," *IEEE Signal Process. Lett.*, vol. 11, no. 2, pp. 112–114, Feb. 2004.
- [19] Z. Wu and N. E. Huang, "A study of the characteristics of white noise using the empirical mode decomposition method," *Proc. R. Soc. Lond. A, Math. Phys. Sci.*, vol. 460, no. 2046, pp. 1597–1611, Jun. 2004.



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